INDIANA HARBOR AND CANAL MAINTENANCE DREDGING AND DISPOSAL ACTIVITIES – DESIGN DOCUMENTATION REPORT

RAILROAD RELOCATION

APPENDIX F

U.S. Army Corps of Engineers, Chicago District Civil Design Section, Design Branch

January 2000

RAILROAD RELOCATION APPENDIX APPENDIX F

TABLE OF CONTENTS

PURPOSE AND SCOPE
GENERAL 1
SITE LAYOUT
General1
Railroad Alignment
Plan/Profile2
PROJECT FEATURES 2
General 2
Ballast System and Roadbed
Design Criteria 3
Project Design Specifics
Drainage Ditch4
Rail Track System4
Horizontal Curves4
Grades and Vertical Curves5
Staging/Storage Areas
MATERIAL QUANTITIES5
General5
Quantities Generation
REAL ESTATE6
CONSTRUCTION SEQUENCE 6
ATTACHMENT 17
Design Criteria
ATTACHMENT 2
Design Calculation and Assumptions
ATTACHMENT 3
Local Sponsor's Concurrence with Preliminary Railroad Relocation Design
LIST OF TABLES AND PLATES
LIST OF TABLES AND TEATES
Table F - 1 Railroad Relocation Material Quantities
Plate F - 1 Typical Cross-sections of Railroad Relocation
Plate F - 2 Plan View of Railroad Relocation
Plate F - 3 Plan and Profile (1 of 4)
Plate F - 4 Plan and Profile (2 of 4)
Plate F - 5 Plan and Profile (3 of 4)
Plate F - 6 Plan and Profile (4 of 4)
Plate F - 7 Cross Sections (1 of 7)
Plate F - 8 Cross Sections (2 of 7)
Plate F - 9 Cross Sections (2 of 7)
Time 1 7 closs bectons (5 of 1)

Plate F - 10 Cross Sections (4 of 7)

Plate F - 11 Cross Sections (5 of 7)

Plate F - 12 Cross Sections (6 of 7)

Plate F - 13 Cross Sections (7 of 7)

Plate F - 14 Soil Borings

Plate F - 15 Real Estate

PURPOSE AND SCOPE

- 1. The purpose of this appendix is to present the design criteria, engineering methods and procedures that were used to prepare a detailed railroad relocation and layout for rerouting the CSX side track crossing the ECI property to the northern portion of the property. This includes establishing the horizontal and vertical alignment, profiles and location of the relocated railroad track, calculating construction quantities and defining the real estate requirements.
- 2. The CSX Transportation Railroad Relocation is being performed as part of the Indiana Harbor and Canal (IHC) and Confined Disposal Facility (CDF) project. The project includes maintenance dredging of the IHC and disposal of the dredged materials in a CDF on the former Energy Cooperative, Inc. (ECI) oil refinery site. The CDF plan includes construction on a portion of the ECI property, which is separated by a 100 feet wide, multiple railroad track ownership/easement corridor. Most of the corridor was abandoned and is presently in use by one lead/side track operated by CSX Transportation. This lead track will be relocated to maximize an optimal dredged sediment placement plan that provides a more economical and constructable CDF design.

GENERAL

3. The project features consist of ballast system and roadbed, adjacent drainage ditches, grading, and slopes required for proper operation of the realigned railway track. The rail track system consists of the track line rails, ties, plates, spikes, anchors, and appurtenant supports. Requirements for implementing this plan include an optimal railway alignment for the relocated track including the curve design as appropriate and required for a single duo rail, side and lead commercial track line to compliment and fit the CDF perimeter, adjacent ditch and groundwater cut-off wall and the extension of the RCRA CAP under the relocated track. The groundwater cut-off wall is required to contain on-site contaminants as well as contaminants from the dredged material. For further information on the groundwater cut-off wall, see Appendix B, "Groundwater Protection". The track design will conform to standard American Railway Engineering Association (AREA) requirements with the first and last 150 to 190 feet of track to be constructed by the railway owners and the track relocation right-of-way (ROW) will not exceed 60 feet. While this appendix provides an overview of the railroad relocation, details regarded the RCRA CAP, the groundwater cut-off wall and utility relocations will be addressed during the preparation of final plans and specification.

SITE LAYOUT

General

4. The site layout design information was developed on a CADD computer system using existing digital topographic and planimetric mapping. All computer work was performed within the Micro-Station software system.

Railroad Alignment

- 5. Calculations to determine the alignment of the proposed Railroad relocation were done with 100' tangents between reversing curves. Existing data was taken from Micro-Station topographic file. An iterative mathematical solution could have been made by hand but given the number of unknowns, a direct solution yielding a 100' tangent was not possible. Further calculations were made by using a computer spreadsheet and GEOPAK COGO. The relocation alignment in the DDR, with respect to the northeast corner of the CDF, differs from that shown on Figure 24 (page 112) of the CMP. The siding now crosses Indianapolis Blvd at 90 degrees. This realignment was necessary so that the existing railroad crossing at Indianapolis Boulevard could be utilized therefore eliminating the need for resurfacing and an extensive new crossing protection system. The revised alignment was designed to maximize space for the CDF while causing minimal or no impacts to Indianapolis Blvd. Plate F-2 shows the railroad relocation layout.
- 6. The solution for the alignment for curves 1 and 2 was obtained graphically in Micro-Station by modifying the arc angle of curve 2 so that a 575 radius curve (#1) could meet a #10-turnout, as provided by the railway owners, where the relocation matches back into the existing rail.
- 7. In order to maximize the amount of space available for the CDF, a trial and error method was used to design curves 3 and 4. The solution that maximizes the area was one that has a 100' tangent between the two 575' (minimum radius) curves 3 and 4. This was obtained using an influence angle, I2 = 79.9d for curve 4 and an influence angle I1 = 51.598d for curve 3. The tangent between the curves is 100.118'. See Attachment 2 for all calculations and assumptions.

Plan/Profile

8. After the alignment was inputted, plan and profiles were derived using existing digital topographic and planimetric mapping. The proposed profile was designed so that the railroad sub-base would not be affected by any surface water runoff. The profile was also adjusted to allow for the design and construction of a 3' RCRA CAP underneath the relocated track within the R.R. ROW. Standard F size sheets (40" x 28") were produced with 1" = 50' scale. These were then reduced to plate size drawings (11" x 17"). Plates F-3 to F-6 show the profile with the corresponding plan view. Plates F-7 to F-13 show cross-sections along the profile.

PROJECT FEATURES

General

9. As discussed before, the project features include the ballast system and

roadbed, adjacent drainage ditches, grading, and slopes required for proper operation of the realigned railway track. The rail track system consists of the track line rails, ties, plates, spikes, anchors, and appurtenant supports. In general, the design of the features follows that which was proposed in the Comprehensive Management Plan (CMP) and the CSX Transportation, Guidelines and Specifications for Design and Construction of Commercial Tracks except for minor modifications based on more detailed design analyses. Each feature will be discussed below.

Ballast System and Roadbed

Design Criteria

- 10. Roadbed width, ditches and slopes shall conform to current CSXT standard roadbed and ballast for industry tracks. This includes 2% subgrade slope, 6" minimum compacted subballast, and 6" minimum ballast at grade point center-line of track. If track is super-elevated then 6" minimum ballast is required below tie under low rail. For cut sections, minimum width of 10' for ditch and 2' for bottom of ditch. Track and ditch gradients may increase ditch size and its distance from centerline of track, and slope can vary as needed for stability from 2:1 in sand to ½:1 in solid rock. For fill sections, slope as required by fill material (1½: 1 maximum) and geotextiles, if used, shall be placed between the top of the subgrade and the bottom of the subballast. Roadbed for commercial trackage within CSXT ROW and parallel to a main or operating track shall be constructed a minimum of 6 inches lower than that of the nearest main or operating track whenever drainage of the existing track can be affected by the new construction.
- 11. Turnout locations require additional roadbed to support the track structure and to provide proper walkways for CSXT train crews. CSXT requires that the roadbed taper from the existing section 100-feet preceding the point of switch (the point at which a track begins to diverge from another) to 18-feet from the centerline at the point of switch. The 18-foot roadbed is to extend from the point of switch to the transition with the 12-foot roadbed on the diverging track.

Project Design Specifics

- 12. The designed ballast system consists of a 9 ½ foot wide standard A.R.E.A. size 4-A ballast on a compacted 12" minimum sub-ballast with a 20-foot wide crest and 2H: 1V side slopes in typical cut cross-sections. 4-A ballast is defined as having 100% passing 2½ "screen size, 90-100% passing 2" screen, 60-90% passing 1½ "screen size, 10-35% passing 1" screen size, 0-10% passing ¾ "screen size and 0-3% passing 3/8 "screen size. Geotextiles are not required. In fill cross-sections, the sub-ballast crest widths vary. The crest width allows for a walkway extended from the centerline of the track on both sides. Plate F-1 shows typical cross-sections.
- 13. The subgrade shall be compacted and finished so that it directs water away from the track. The design slope is 2% from the centerline of the track on both sides. See Attachment 2 for all calculations and assumptions.

Drainage Ditch

- 14. The drainage system is sized to carry drainage without ponding of water against the roadbed. The ditch is designed to contain the drainage water as it filters into the site as normal. Drainage shall not be diverted, directed toward CSXT, or increased in quantity without prior approval and agreement with CSXT. Track roadbeds fills shall not be used as dams or levees for retention of water nor shall CSXT ROW be utilized for retention or settling basin.
- 15. The designed side slopes of the drainage ditch are 3H:1V with a 2-foot depth and 3-foot bottom width for constructability (Plate F-1). The profile was also raised so that the entire typical section is above the existing ground line.

Rail Track System

16. The rail track system consists of the track line rails, ties, plates, spikes, anchors, and appurtenant supports. The controlling elevation was the existing track elevations at the west and east ends of the project site. Curve information for each curve includes the intersection angle, degree of curve, radius, tangent distance, external and length of curve. Plate F-1 shows cross-sections of the rail track system.

Horizontal Curves

- 17. Trackage was designed using the minimum degree (maximum radius) of curve practicable. It is typical to use the chord definition of the degree of curve, which is defined as the central angle subtended by a 100 foot chord. It is denoted by Dc, where $\sin \frac{1}{2} Dc = 50/R$. Wherever practicable, a curve should begin beyond the last switch tie, but if required by special circumstances, a curve may extend onto the switch ties. In no case shall a curve begin between the point of switch and the heel of frog (the end of the point at which two running rails intersect within a turnout or crossing that is furthest from the point of switch).
- 18. A curve should be avoided at the loading point of a bulk loading facility or at an under track unloading structure. Spiral curves and super-elevations are not normally required, but, if required by special circumstances, shall be designed according to current CSXT standards. Tangents (straight sections), as specified in Attachment 1 Design Criteria, shall separate reverse curves (curves following each other in opposite directions).
- 19. The designed curves met the above criteria. As stated earlier, the designed alignment for curves 1 and 2 was obtained by modifying the arc angle of curve 2 so that a 575 radius curve (#1) could meet the #10-turnout. The design for curves 3 and 4 was one that has a 100.118' tangent between the two 575' (minimum radius) curves 3 and 4. Additional information is provided on plate F-2. See Attachment 2 for all calculations and assumptions.

Grades and Vertical Curves

- 20. Track grades are to the minimum possible, consistent with terrain requirements. Grades were carefully designed to ensure that motive power available will handle the tonnage to be moved. This takes into consideration number of cars, whether loaded or empty, etc. Grades for "Load / Unload in Motion" trackage were designed so that a train is under power with no bunching of couplers while loading or unloading.
- 21. Frequent changes of grade were avoided. Vertical curves were provided at all grade changes, and were as long as practicable. Minimum standards for calculation of vertical curves are specified in Attachment 1, Design Criteria. Neither grade changes nor vertical curves are within the limits of switch ties. The designed curve information is provided on plate F-2. See Attachment 2 for all calculations and assumptions.

Staging/Storage Areas

22. Staging/storage areas are provided within the existing CSXT ROW as shown on plate F-2. Details will be finalized during the preparation of plans and specifications.

MATERIAL QUANTITIES

General

23. Quantities were either manually calculated or computer calculated using the InRoads or MicroStation software. They consist of track complete in place, ballast, subballast, earth excavation, embankment, concrete removal, furnishing and placing topsoil and seeding, existing track to be removed, existing topsoil to be stripped, clay cap and #10 turnouts. The quantities are presented in table F-1.

Quantities Generation

24. Earthwork volume quantities include earth excavation, embankment and clay cap. Track complete in place length was taken between the stations 69+60.81 and 97+59.19. Ballast and sub-ballast tonnage was calculated. Concrete removal was calculated by taking the area of the concrete to be removed at a depth of 1 foot. Furnishing and placing topsoil and seeding was determined from the length of the relocation and the ROW with an allowance for the track complete in place to be installed. Track to be removed is assumed to be two complete sets of track line and includes removal of all tracks material and ties while existing ballast material will remain. All removed material is to be stockpiled on site. All removed material remains the property of the railroad and is stored for railroad pickup. Topsoil to be stripped was determined from the length of the relocation and the ROW Clay cap was determined from the ROW to the cut-off wall.

REAL ESTATE

25. Total land required for the railroad relocation is 4.11 acres. The real estate required for the track relocation and CAP requirements temporary work limits is equal to the permanent easements for the relocated track. All land required for the project is owned by the Non-Federal Sponsor except for ROW easements owned by the railroads. Plate F-15 shows the real estate for the railroad relocation.

CONSTRUCTION SEQUENCE

26. The first feature of the project to be constructed is the relocated railroad track. The RCRA cap will be installed within the relocated R.R. ROW. The sub-ballast and ballast system will be installed and then the railroad track will be constructed. Topsoil and seeding is done to complete the relocation work. As the relocated railroad track is brought on line, the existing track shall be abandoned. After the existing line is abandoned, the ROW will be stripped and excavated.

ATTACHMENT 1

Design Criteria

Design criteria to be used for sidetracks with operating speeds no to exceed 15 mph are listed in the following table. The criteria are not intended for Yard and Terminal track, Intermodal track, Branch or Spur Lines, or any trackage with operating speed greater than 15 mph.

CRITERIA	INDUSTRY TRACK	LEAD TRACK	LOAD / UNLOAD IN
m			MOTION
Turnout Size			
	Number 8	Number 10	Number 10
Note: turnouts in main			
tracks shall be No. 10			
or larger			
Maximum Curves			
Degree	12d-00'-00"	10d-00'-00"	10d-00'-00"
Radius	478.34'	573.69'	573.69'
Tangent Between			
Reverse Curves			
Preferred	100'	100'	
Minimum	60'	60'	100'
Maximum Grade			
Loop Track	2.5%*	2.5%*	1.5%*
* Uncompensated			
** Compensated at			0.7%**
0.04% per degree of			
curve			
Vertical Curve			
Summits	40 x algebraic	40 x algebraic	400 x algebraic
	differences in grades	differences in grades	differences in grades
	5		
Sags	50 x algebraic difference	50 x algebraic difference	500 x algebraic
	in grades	in grades	difference in grades
	<i>6</i>	6	
Length	100' minimum	100' minimum	100' minimum

ATTACHMENT 2

Design Calculation and Assumptions

URS Greiner Woodward Clyde CALCULATION COVER SHEET

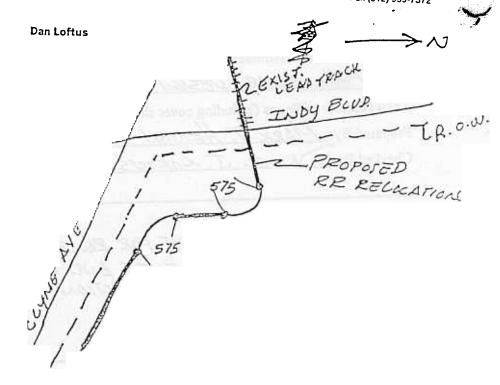
Client: USACOE Project Name: C	SXTRACK RELOCATION
Project/Calculation Number: 05-0003547	7.19
Title: FRELIMINARY DESIGN CALCULATION	ONS AND QUANTITY TAKEOF
Total Number of Pages (including cover sheet):	-
Prepared By: MARK T. HEATON	Date:
Checked By: JANIEZ J. LOFTUS	Date:
Description and Purpose: DEVELOP AN ALIGNMENT FOR PANCE ADDESSES CEXT COMMENTS AND REMAINDER FOR CDF CONSTRUCTION	MBXIMIZES SITE
Design bases/references/assumptions: O TOPO/CONTAIRS AND PREJIM. ACIENTA O CONTAIRS AND PREJIM. ACIENTA O COMPUTER GENERATED QUANTITY/DESIGN USING MICROSPATION/EOPAK.	ED BY RENZOAD ERNA 1946
Remarks/conclusions: ① HORIZONTAL ANGNMENT MEETS BOTH & ② PZELIM. REVIEW OF AUGNMENTS INDICA REQUIRED PRIOR TO CONSTRUCTION, BUT IS ACC ③ UTICITY CONFLICTS NOT SHOWN IN CALC APPROVAL OF PREUM. BLIGHMENTS.	LIE MINOR MODIFICATIONS BRE CEPTABLE (e.g. 200'V-CE/10°CURVES
Calculation Approved By:	Date:
Project Manag	
Revision No.: Description of Revision:	Approved By:
	Project Manager/Date



01/08/99

Engineers • Architects • Planner 122 South Michigan Avenue Suite 1970 Chicago, Illinois 60603 (312) 939-7704 Fax (312) 939-7372

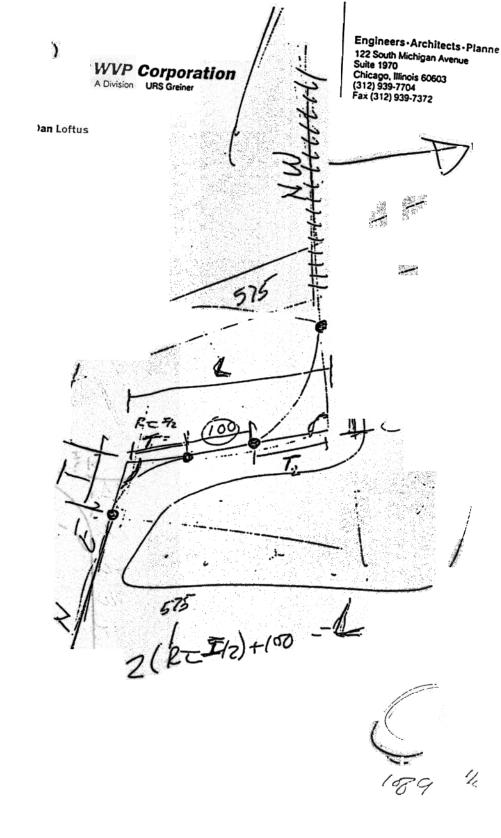
WVP Corporation "A Division of URS Greiner



CALCULATIONS TO DETERMINE
ALIGNMENT OF PROPOSED RR
RELOCATION WITH 100' TANGENT
BETWEEN BEVERSING CURVES.
EXISTING (GIVEN) DATA TAKEN FROM
TO PO FILE (MICROSTATION).

PREPARED BY: DAN COFTUS

DATE: 01/11/99





... WVP Corporation
A Division of URS Greiner

Engineers - Architects - Planne 122 South Michigan Avenue Suite 1970 Chicago, Illinois 60603 (312) 939-7704 Fax (312) 939-7372

Dan Loftus

T=Rook 2I

207904

WVP Corporation

** A Division of URS Greiner

Engineers · Architects · Planns 122 South Michigan Avenue Suite 1970 Chicago, Illinois 60603 (312) 939-7704 Fax (312) 939-7372

Dan Loftus

28.302

61.0EN

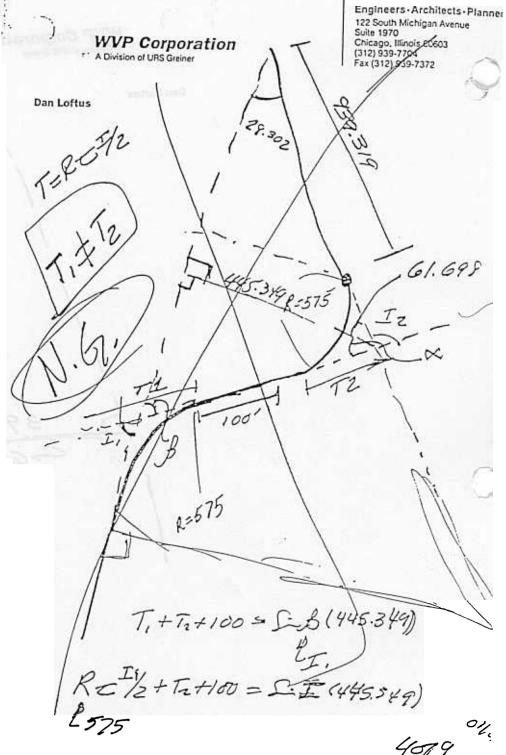
65.65

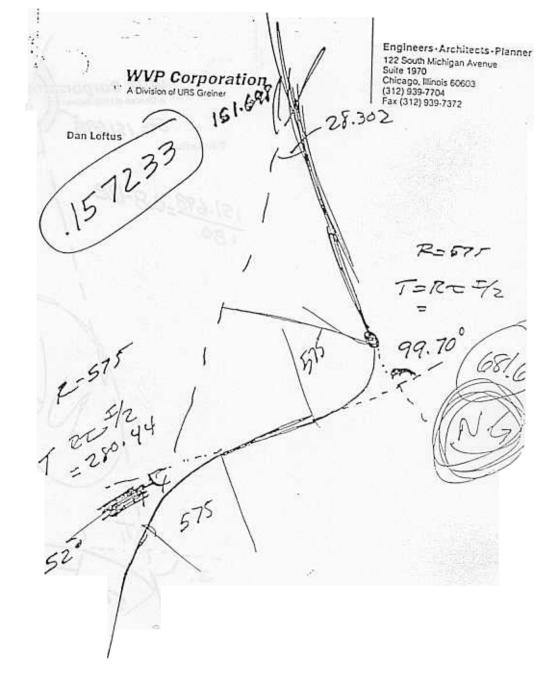
61.0EN

61.0EN

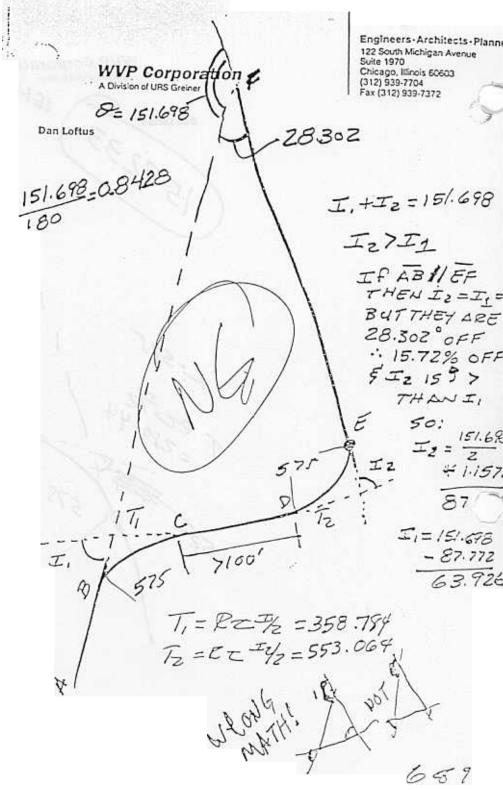
61.0EN

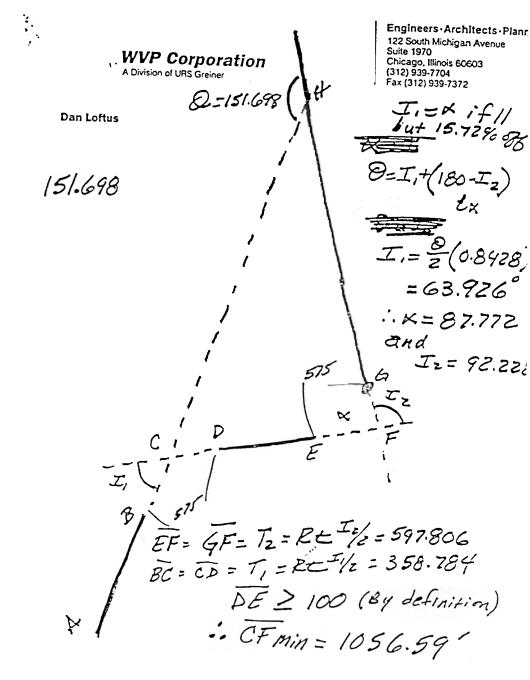
389016





2899 a16



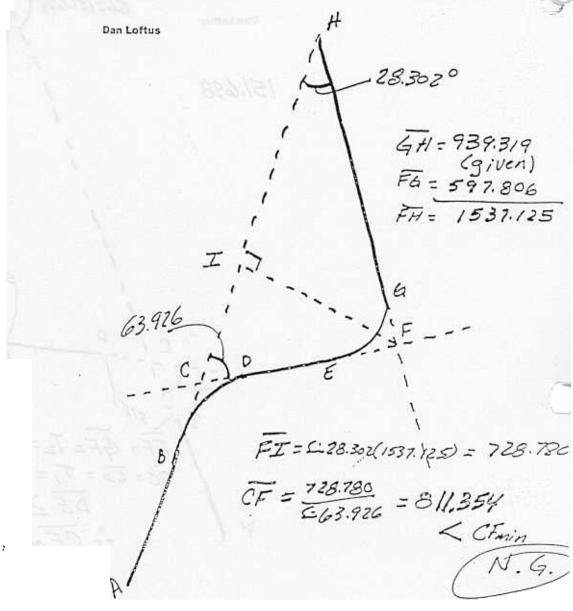




Engineers · Architects · Planner: 122 South Michigan Avenue Suite 1970 Chicago, Illinois 60603

Suite 1970 Chicago, Illinois 60603 (312) 939-7704 Fax (312) 939-7372

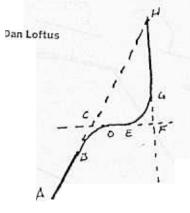
WVP Corporation
A Division of URS Greiner



15.72% split
assumption
N.4.

Engineers - Architects - Planner 122 South Michigan Avenue Suite 1970 Chicago, Illinois 50603 (312) 939-7704 Fax (312) 939-7372





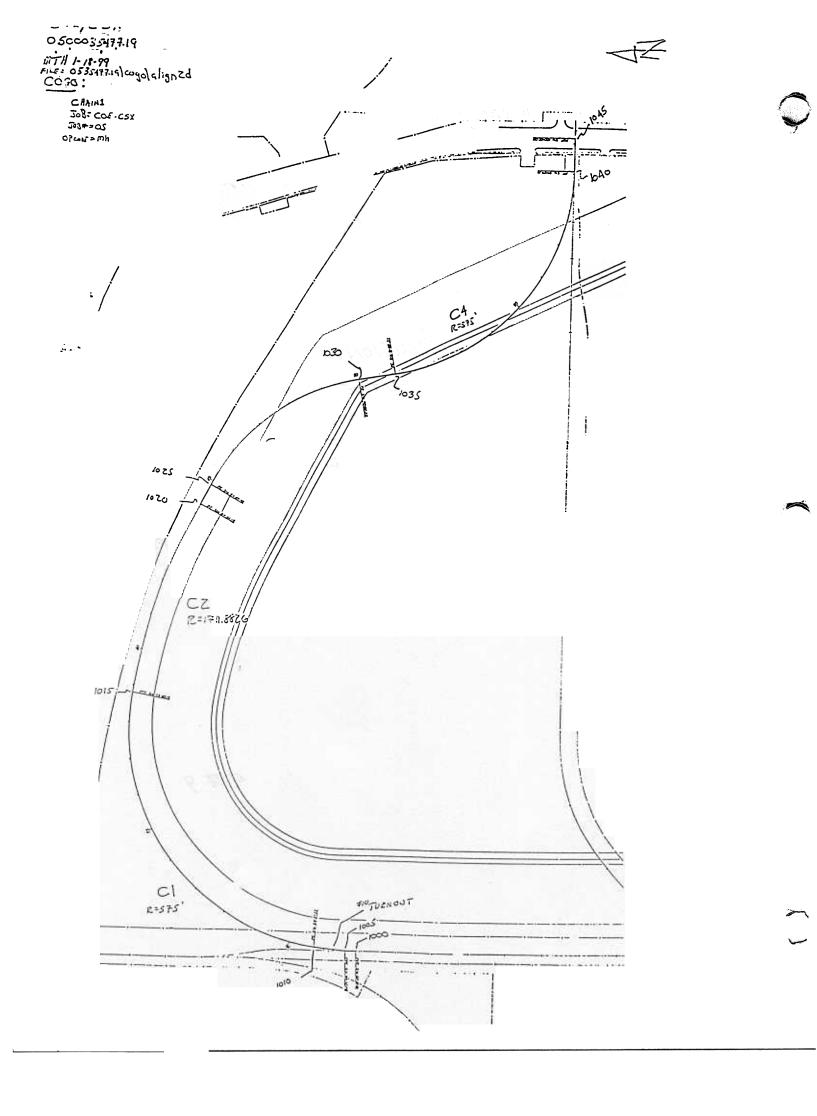
• •

CF=T, +Tz +100 =(REJ,)+RE=z)+100

CONCLUSION:

AN ITERATIVE MATHMATECAL SOCYTION
COULD BE MADE BY HAND, BUT GIVEN
THE NUMBER OF UNKNOWNS A DIRECT
SOLUTION SIELDING A 100.00 FOOT
TANGENT (DE) IS NOT POSSIBLE. FURTHER
CALCULATIONS WILL BE MADE USING
COMPUTER SPREADSHEET OR GEOPAK COGO.

9079



Job COF/CSX	Project No. <u>Q5-000 35477, 19</u>	Page/_ of
Description Track Relocation Algorithm	Computed by	
SPINE TO THE PROPERTY OF THE P	Charled by	Date//
TRIAL É ERROR FOR CURVES F (GH = 939319 MESSURA L'IN MICROSINIEN CES.301° E	E=Z R=575'	Referen
, G DC -	$= \overline{GF} = T_{Z} = R + \epsilon_{D}^{T_{Z}} / 2$ $= \overline{CD} = T_{I} - \overline{E} + \epsilon_{D}^{T_{I}} / 2$ $= \overline{CD} = T_{I} - \overline{E} + \epsilon_{D}^{T_{I}} / 2$	
I. 5' - 6 F IF AT DE	= 100 = min tryent letwer	the E. curre
6/	(CSX standards) It the one for the Combin	els- 1.11
$T_{1/1} = \frac{95^{\circ}}{z_{1}}$ $T_{2} = \frac{95^{\circ}}{5}$ $T_{3} = \frac{95^{\circ}}{5} + \frac{15}{2} = \frac{627.502}{25}$ $0 = \frac{95}{25}$ $T_{4} = \frac{95^{\circ}}{5} + \frac{15}{2} = \frac{166.698}{66.698} = \frac{57}{7}$ $T_{5} = \frac{378.409}{5}$	NO GOOD	
T2: 482.482 9: 100	NO 6002	
I, = 51.698 T1 = 278.573	DF 7/00 153 198-100	
3) Try IIz = 750! Tz: 575-ton 52/2 = AA1. 213 = 0 = 105°	72 NO GOG:	
W - 103	VO 0003	
I, = 16.6 98	DE >100	

URS Greiner Woodward Clyde

Job COI-/CSX _____ Project No. ___

_____ Computed by MTH

Sheet ____ of _

Description ____

(:

Date

CURVES 122 Checked by _____

Reference

TRY /= 7950/ Tz = 478.222 d = 100.5

Na Caoq

DE >100

I.= 51.198 Ti= 275.481

TRY Iz = 75.8 Tz= 480.775 a = 100.Z

NO GOOD

12.769 : DE > 100

I, = 51.498 TI = 277.335

TRY I = 80.5 Tz = 480.7 = 3 4= 99.5

NO 600 D

DEL100 by 12.693

工,= 57.198 T, - 281.677

Try Iz = 79.9 Tz = 481.628 a = 100.1

Ves

DE = 100.118 = 100.

I.= 51.57F T= Z77,953

URS Greiner Woodward Clyde

Job COE/CSX	Almand A Secure Control of the Control of the	Page of
	Project No.	Sheet of
Description HOLIBONTAL ALIGNMENT FOR CURVES 3 F4	Computed by MTH	Date _/-/4-99
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Checked by	Date

Reference

CONCLUSION.

IN ORDER TO MAXIMIZE THE AMOUNT OF SPACE AVAILABLE

FOR THE CONFINED DISPOSAL IMCILITY, A TRIAL SERROR

METHON WAS USED TO DESIGN CURVES 3 & A. THE SOLUTION

THAT MAXIMIZED THE AREA IS ONE THAT HAS A 100'

TANGENT BETWEEN THE TWO 575' (MIN RAD.) CURVES (3 & A).

THIS WAS OCTAINED USING AN INFLUENCE ANGLE, I; 79.9°,

FOR CORVE A & AN INFUENCE ANGLE, I, = 51.598° FOR

CURVE 3. THE TANGENT BETWEEN THE CURVES IS

100.118'

Job COE/CSX Description HORIZONIAL ALIGNMENT FOR CUPUES 12 Z	Project No Computed byH Checked by	Page of Sheet of Date Date
TRIAL 1	(CURVES 122)	Reference
X=87. 4879 I= 92.5721 T=575 Int 2 600 180	NO 600D	
Musule T = 602.0551		
7×12/2 d: 87.1427 I= 92.8373 F/2=46.419		
TRIAL =3 L = &5.7978 L = 94.7072 =12-47.1011 T = 618.798		
TRIAL#4	= 6 ! T. X	

x= 85.4717 I= 94.5783 I/z = 47.789 T = 627.885 R= T/+on T/2= 565.009 => R = +0= 500

No & Good

Job	13	Page	
Description	Project No	Sheet	
CURVEC 17, 2	Computed by MTH	Date	17
Alexander of Co	Checked by	Date	
TRIALES	The second secon		R
1 617 445			
d 84.7255			
95 7745			
F/2 7.657	,		
Mucred 619. 724	No	Go	زخز
R T/ter 12 365 47 .	> too 5 11		
Mark on .	च्या विकास करते । च्या विकास		
TRIAC IIG			
82.2926	.1/		
I 7.7074	NO 600D		
The 48 \$537	"(
Mass 618.65 45		r	
R			
	F		
(Now broken Von 1 TORDONT Sto)	pf.		
TRAL =7	<i>k</i>		
× 291			
F 9 7087			
ton I/z 4447			
	\		
575 ten3/2 & 357	250		
Messured 7 6 1398			
pc 610 80		_	
		-	,.
FRIAL #-8			

Oi.

 \bigcirc

URS Greiner Woodward Clyde	·		
		Page of	
Job Coi/csx	Project No	Sheet of	-
Description HOPIZ. ALIKAMENT FOR	Computed by	Date 11-13-96	-
(09.025 17.7	Checked by	Date	
		Reference	

WMUST USE TRIAL É ERROR METHOD: CRAPHICACLY IN MICROTATION IN ORDER TO COT CURVE # 1 to MEET the \$10 TURNOUT

CONCLUSION

{

THE SOLUTION FOR THE ASIGNMENT FOR

CURVES IR Z LUMS CETAINED GRAPHICALLY

IN MICCOSTATION BY MODIFFIED THE ARC ANGLE

OF CURVE Z (GIVEN TO US BY COE) SO THAT

A STS RAS. CURVE HI COULD MEET A # 10

TURNOUT WHERE THE RELECATION MATCHES

BACK IALTO & KISYN, RAIL.

und Greiner Woodward	d Clyde		
Job COE/CSX Description VERTICAL CURVE 16		Project No	Page of Sheet of Date Date
			Reference

CSX STANMED SPECES.

115#

25.625 = 1.625

25.625 = 1.76775

31.625

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.76775

25.625 = 1.7677

Design Proposed vertical profile to be approx 57.4 cs" above existing profile in order to minimize Cuts & fills.

Copyright (1993) GEOPAK Corporation

All rights reserved

Project: coe-csx Subject: alignment

Job No. 05

Operator: NH Wednesday January 20, 1999 11:07 am

Date:

SYSTEM FIX 4 ASEC 2 BEAR PRI 0 NOR NE STA 2 FILE: 'CHAIN'

Describe Chain CHAIN1

Chain CHAIN1 contains:

1000 1005 CUR C1 CUR C2 CUR C3 CUR C4 1045

Beginning chain CHAIN1 description

Foint 1000 N 1,513,722.6010 E 389,157.8190 Sta 68+10.81

GEOPAK

Tourse from 1000 to 1005 N 0" 22' 26.48" E Dist 31.2507

N 1,513,753.8510 E 389,153.0230 Sta 68+42.06

Course from 1005 to PC C1 N 6" 00' 52.95" E Dist 85.7099

Curve Data *-----

Durve Cl						
P.I. Stati	ion	75+54.21	N	1,514,462.0793	Ε	389,232.6434
Delta	•	94~ 54' 11.54"	(RT)			,
Digree	-	9" 57' 52.14"				
Tangent	-	626.4392				
Length	• , 1.	952.4147				
Redius	•	575.0000				
External	-	275.3241				
Long Chord	-	847.2124				
Mid. Ord.	-	185.1777				
P.C. Stati	lon	69+27.77	N	1,513,839.0890	Ε	389, 7.0040
P.T. Stati	on	73+80.19	N	1,514,343.4320	Ε	389, 7.7440
T.C.			N	1,513,778.8395	Ε	389,8363
Back	- 1:	6" 00' 52.52" E				
Ahead	- S	79° 04' 55.94" E	,			
Thord Bear	- N	53° 27' 58.29" E				

Curve Data *-----

Crine C3	,				
P.I. Station	81+57.71	H	1,514,290.8692	Ε	390,120.2438
Delta =	19~ 25' 00.71"	(RT)	•	_	0,0,220.2130
Degree =	3" 20' 49.00"				
Tangent =	277.5230				
Length =	550.2588				
Radius =	1,711.8826				
External =	22.3495				
Long Chord 🐷	547.8930				
Mid: Ord. =	22.0615				
P.C. Station	78+80.19	N	1,514,343.4320	E	389,847.7446
P.T. Station	84+30.44	N	1,514,154.9080	_	390,362.1810
c.c.		N	1,512,662.5344		•
Back ■ S	79^ 04' 56.03" E		1, 4, 002. 3344	E.	389,523.5135
	60° 39' 55.33" E				
Chord Bear - S	69° 52' 25.63" E				

Course from PT C2 to PC C3 S 60° 61' 51.80° E Dist 53.9599

1s this corrent print

Nost 2000 pater

Plans

Plans

Lizzlaa

Plans

Lizzlaa

JAINE C3				· •		
'.I. Stat	ion	87+67.35	N	1,513,990.0186	E !!!	390,655.9835
)#lta	•	51 35' 50.88"	(RT)		_	3,0,633.9835
र्की । } १ । ४	•	9 57' 52.14"				
ing At	-	277.9502				
Length	-	517.8138				
iadius	-	\$75.0000				
External	-	63.6559				
Long Chord	•	500.4929				
d. Ord.	-	57.3112				
'.C. Stat	ion	84+89.40	N	1,514,126.0520	E	300
'.T. Stat:	ion	90+07.22	N		E	390,413.5970
:.c.			N		_	390,699.9450
ack	- S	60° 41' 51.96" E	.,	1,513,624.6231	E	390,132.1825
Phead	- S	9" 06' 01.08" E				
mord Bear	- s	34" 53' 56.52" E				

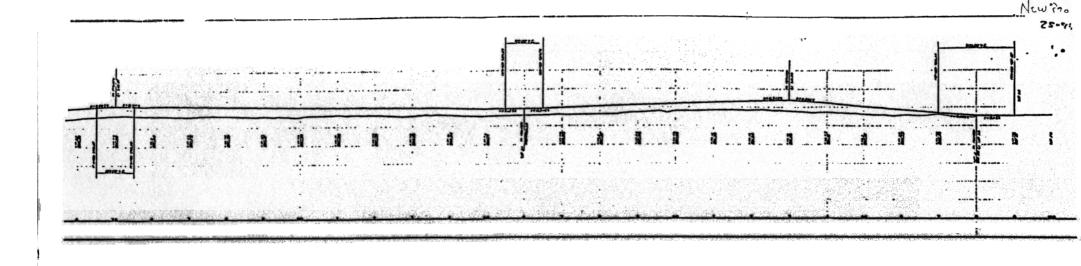
Curve Data

Turve Ce		•••••	•••••		
urve C4 .I. Station elta = egree = angent =	95+88.97 79 ⁻ 53' 59.74* 9 ⁻ 57' 52.14* 481.6272		1,513,141.1403	E	350,791.5591
adius .xternal .ong Chord .cid. Ord	501.8472 575.0000 175.0558 736.4361 134.2016				
	99+09.19 9° 06' 01.67" E 69° 00' 01.41" E 49° 03' 01.54" E	N N	1,513,616.7050 1,513,132.7360 1,513,707.6505	E E	390,715.7820 391,273.5130 391,283.5442

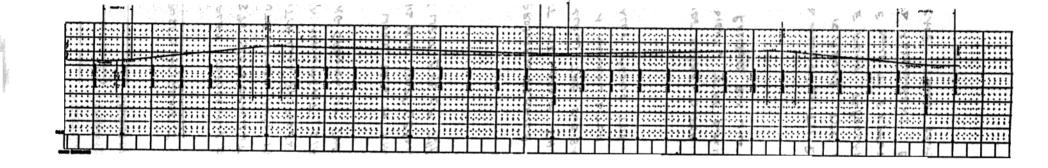
Durse from PT C4 to 1045 S 86° 59' 59.58" E Dist 90.8078

pint 1045 N 1,513,13k.1530 E 351,364.3070 Sta 100+CG.00

ding chain CHAIN1 description



OLD PROFILE



URS Greiner Woodward Clyde

Job_COE/CSX	Project No.	Sheet	of
Description DRAINAGE DITCH	Computed by MTH	Date	7-10-88
	Checked by	-Qate	

DRAINAGE DITCH ALONG PROPOSED ALIGNMENT

see comments Reference on plans regarding drainage ditch(es)

DUE TO THE VERY FLAT TOPOGRAPHY OF THE SITE A DITTALITH SITE A DITTALITH SITE A DITTALITH SITE A DITTALITH SITE SIDES OF SLOPE GRADIENT & A 1 FOOT MINIMUM DEPTH WAS PROPOSED TO ROUTE WATER AWAY FROM THE TEOPOSED PAUROAD ALIGNMENT. THE DITCH WAS PROPOSED TO RUN ALONG THE SOUTH SIDE OF THE PROPOSED ALIGNMENT, STARTING AT THE EAST END AND MATCHING EXISTING GROUND AT THEWEST END.

THIS DID NOT WORK DUE TO THE EXTREMELY FLAT TOPOGRAPHY.

A DITCH WITH THIS MIN. YOPE GRADIENT WOULD NOT MATCH

EXISTING AT THE WEST END OF THE PROPOSED & ALIGNMENT.

SOLUTION:

- TRAISE THE PROPOSED PROFICE SO THAT THE TYPICAL
 SECTION IS AT OR ABOVE THE EXISTING GROUND LINE.
 THIS WOULD ALLOW THE SUB-BACLAST TO ACT AS THE
 SIDE SLOPE OF A NATURAL DITCH & THE WATER WOULD
 FLOW NATURALLY ALONG THE PROPOSED ALIGNMENT
- OUSE A 3:1 SIDE SLOPE DITCH WITH A ZFOOT DEPTH &

 NO SLOPE GRADIENT. THE DITCH WILL CATCH ANY RUNDER

 THAT THE RAILROAD BED WILL NOT BE AFFECTED.
- FOLUTION D WAS USED ALONG WITH RAISING THE PROFILE SO THAT
 THE ENTIRG TYP. SECT. IS ABOVE THE EXISTING & GROUND LINE.

 THE ENTIRG TYP. SECT. IS ABOVE THE EXISTING & GROUND LINE.

 THE BECAUSE OF THE FLAT TO POGRAPHY & THE SANDY SOILS

 (BORING LOGS) THE WE DON'T EXPECT MUCH RUNGER IN THE

 AREA OF THE PROPOSED ALIGNMENT, BUT THE DITCH IS A

 SAFEGUAR'S IN THE CASE THAT SOME RUNDER OCCURS.



Table F - 1 Railroad Relocation Material Quantities

Item	Unit	Contractor	Railroad	Total Quantity
Track Complete in	LINEAR FEET	2,798	183	2,981
Place				
Ballast	TONS	1,628	104	1,732
Sub-Ballast	TONS	6,029	692	6,721
Earth Excavation	CUBIC YARDS	4,926	0	4,926
Embankment	CUBIC YARDS	0	0	0
Concrete Removal	SQUARE YARDS	476	0	476
Furnishing and	SQUARE YARDS	15,260	0	15,260
Placing Topsoil				
and Seeding				
Track to be	LINEAR FEET	5,321	0	5,321
Removed				
Topsoil to be	SQUARE YARDS	21,662	0	21,662
Stripped				
Clay Cap	CUBIC YARDS	18,720	0	18,720
#10 Turnout	EACH	Q	1	1
Silt Filter Fence	FOOT	4,080	0	4,080

URS Greiner Woodward Clyde			
Job <u>COF/CSX</u>	Project No	Page Sheet	·
Description PROFILE & CROSS SECTION CHANGES			of _ <i>5/17/9</i> 9
FOR BACKSHEEK SUBMITTAL PER 10090 CONNER		Date	
			Reference

PROFILE WAS RAISED A TO ALLOW FOR A Z'RCRA CAP TO BE
PLACED THROUGHOUT THE GO' IC. FASEMENT. THE NEW GUANTITIES
ARE SHOWN ON THE FOLLOWING PAGE



· CROSS SECTIONS WERE RECUT @ 5 INTHE BOTH THE VERTICAL &
THE HORIZONTAL. TOPSOIL, STRIPPING & REGRACAP SHOWN IN ALL CROSS
SECTIONS

THE DITCH WAS CHANGED FROM A 1' BOTTOM TO A 3' BOTTOM FOR CONSTRUCT ABILITY

COE/CSX TRANSPORTATION TRACK RELOCATION AT THE INDIANA HARBOR CONFINED DISPOSAL FACILITY



Project #: 0500035477.19 Computed by: MTH July 14, 1999

SUMMARY OF QUANTITIES

ITEM	UNIT	TOTAL QUANTITIES	CONTRACTOR	RAII ROAD
ITEM	UNIT			
TRACK COMPLETE IN PLACE	L.F	2981	2798	183
BALLAST	TONS	1732	1628	104
SUB-BALLAST	TONS	6721	6029	692
EARTH EXCAVATION	CU. YD.	4926	4926	0
EMBANKMENT	CU. YD.	DAS I DO THAT	46.00	Thos Oak
CONCRETE REMOVAL	SQ. YD	476	476	0
FURNISHING AND PLACING	SQ. YD	15260	15260	0
TOPSOIL AND SEEDING				
TRACK TO BE REMOVED	L.F.	5321	5321	0
TOPSOIL STRIPPING	SQ. YD.	21662	21662	0
CLAY CAP	CU. YD.	18720	18720	377 O2
#10 TURNOUT	EACH	1	0	1
SILT FILTER FENCE	FOOT	4080	4080	0



COE/CSX TRANSPORTATION TRACK RELOCATION AT THE INDIANA HARBOR CONFINED DISPOSAL FACILITY

PROJECT #: 0500035477.19
DESCRIPTION: CUT AND FILL QUANTITIES

COMPUTED BY: MTH.

DATE:

May 21, 1999

AVG VOLUME (cy) = [D(A1+A2)/2)/27

A1=AREA1 (sf) A2=AREA2 (sf)

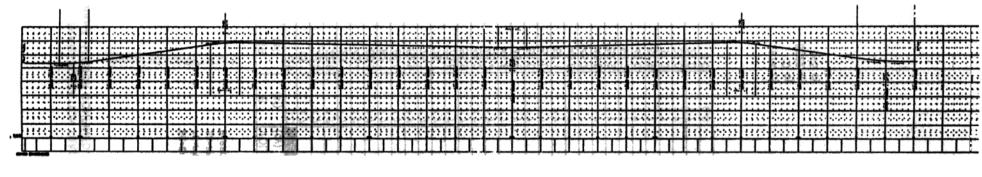
DEDISTANCE BETWEEN AREAS

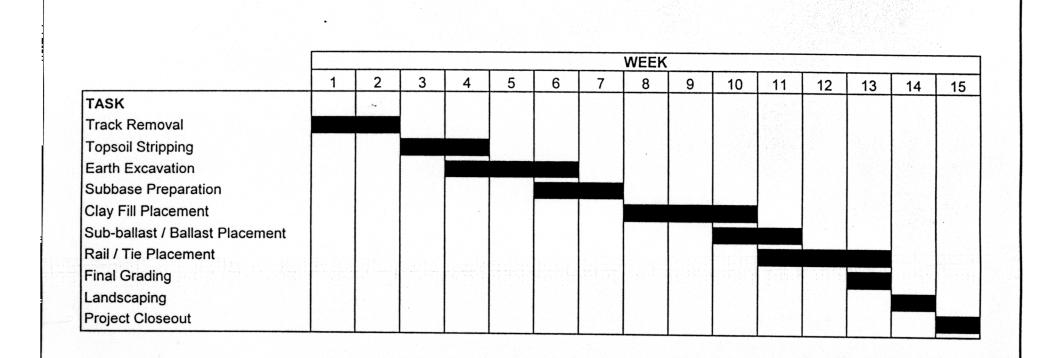
EE=EARTH EXCAVATION
FE=PROPOSED EMBANKMENT
SB=PROPOSED SUB-BALLAST
B=PROPOSED BALLAST

STA	EE (sf)	EMB (sf)	SB (sf)	B (sf)	VOL EE (cy)	VOL EMB	VOL SB (cy)	VOL B
6810.811	0.0	0.0	0.01	0.0		TO SECURE	Coyl	Cy /
6900	48.1	0.0	13.1	4.7	79.4	0.01	21.6	7.7
7000	60.0	0.0	22.0	7.7	200.1	0.0	0.01	22.9
71001	96.7	0.0	22.01	7.7	290.2	0.0	81.5	28.5
7200	7.31	0.0	23.1	7.7	192.6	0.0	83.51	28.5
7300	7.11	0.0	43.4	7.7	26.7	0.01	123.11	28.5
7400	6.9	0.0	60.51	7.7	26.0	0.0	192.4	28.5
7500	6.9	0.0	82.7	7.7	25.6	0.0	265.11	28.5
7600	7.01	0.0	86.01	7.7	25.7	0.0	312.31	28.5
7700	7.01	0.01	82.9	7.7	25.9	0.0	312.8	28.5
7800	6.5	0.0	76.7	7.7	25.0	0.01	295.61	28.5
7900	6.7	0.0	76.1	7.7	24.4	0.0	283.01	28.5
8000	7.7	0.01	73.8	7.7	26.7	0.01	277.61	28.5
8100	6.7	0.0	56.9	7.7	26.7	0.01	242.0	28.5
82001	6.71	0.01	55.2	7.7	24.8	0.0	209.41	28.5
8300	7.11	0.0	56.4	7.7	25.6	0.01	208.51	28.5
8400	6.9	0.0	46.8	7.7	25.9	0.01	191.11	28.5
8500	7.01	0.0	48.9	7.7	25.7	0.01	177.21	28.5
8600	7.01	0.01	51.01	7.7	25.9	0.0	185.01	28.5
8700	7.61	0.01	50.01	7.7	27.0	0.01	187.01	28.5
88001	6.81	0.01	57.11	7.7	26.7	0.0	198.31	28.5
8900	7.21	0.0	48.8	7.7	25.9	0.01	196.11	28.5
90001	6.61	0.01	45.7	7.71	25.6	2.01	175.01	28.5
91001	6.91	0.01	48.81	7.7	25.0	0.0	175.01	28.5
9200	7.3	0.0	52.9	7.7	26.3	0.01	188.3	28.5
9300	5.81	0.0	52.2	7.7	24.3	0.01	213.11	28.5
9400	6.1	0.01	42.0	7.71	22.0	0.01	193.01	28.5
9500	138.9	0.0	67.9	7.7	268.5	0.01	203.51	28.5
96001	147.7	0.01	37.3	7.7	530.8	0.0	194.81	28.5
97001	190.81	0.0	22.0	7.7	626.9	0.01	109.81	the second secon
98001	224.21	0.01	22.01	7.7	768.4	0.0		28.5
9909.19	6,01	0.0	0.0	0.0	453.21	0.01	81.5 44.5	28.5 15,5
					3973.6	0.0	5521.9	844.6

TOTAL EARTH EXCAVATION: 3974 cy
TOTAL EMBANKMENT: 0 cy
TOTAL SUB-BALLAST: 5622 cy
TOTAL BALLAST: 845 cy

RB





Prepared By:

URS Greiner Woodward Clyde



US Army Corps of Engineers CSXT Track Relocation at the Indiana Harbor CDF

Construction Sequence Schedule



ATTACHMENT 3

Local Sponsor's Concurrence with Preliminary Railroad Relocation Design



VICE-PRESIDENT EDWARDO MALDONADO PRESIDENT FRANK KOLLINTZAS

EXECUTIVE DIRECTOR
ADRIANE ESPARZA

ROBERT A. PASTRICK MARINA 3301 ALDIS AVENUE EAST CHICAGO, IN 46312

June 10, 1999

Sterling Johnson, ED-DC US Army Corps of Engineers 111 N. Canal Street, Suite 600 Chicago, IL 60606

Re: CSX Transportation Track Relocation at the Indiana Harbor Confined Disposal Facility

Dear Mr. Johnson:

The East Chicago Waterway Management District has reviewed the final design memorandum for the above project and has no additional comments.

Sincerely,

Adriane Esparza

AE/ae

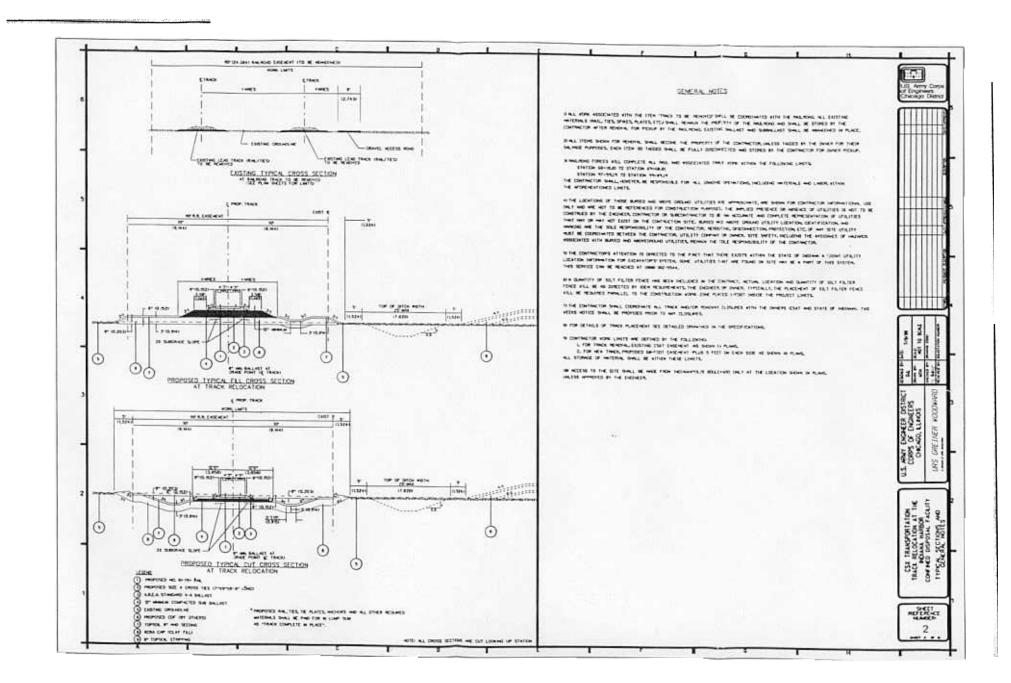


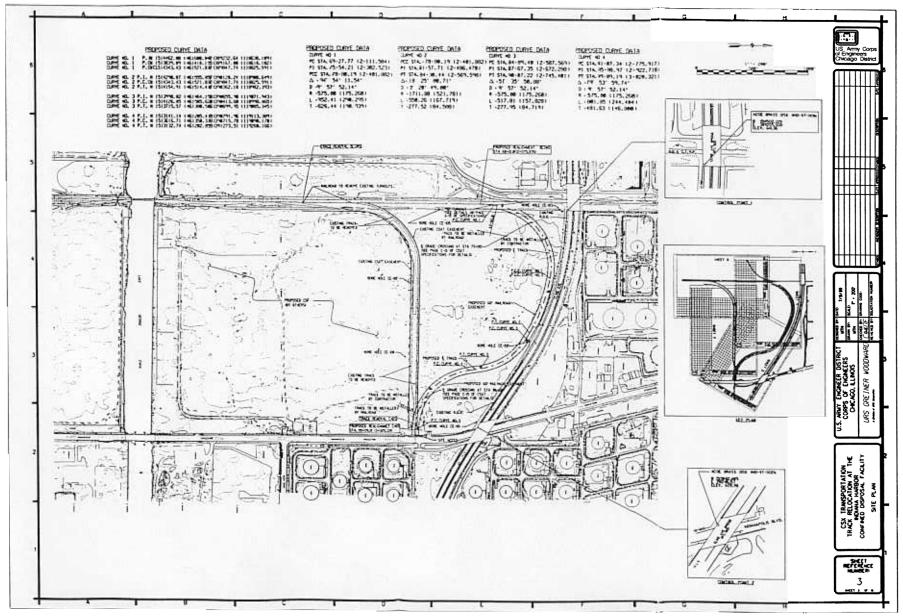


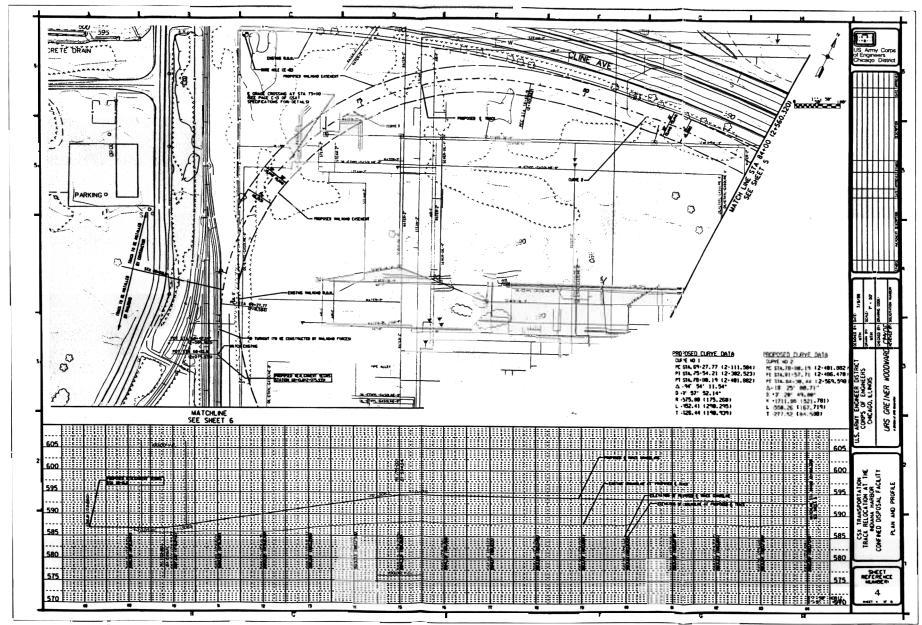


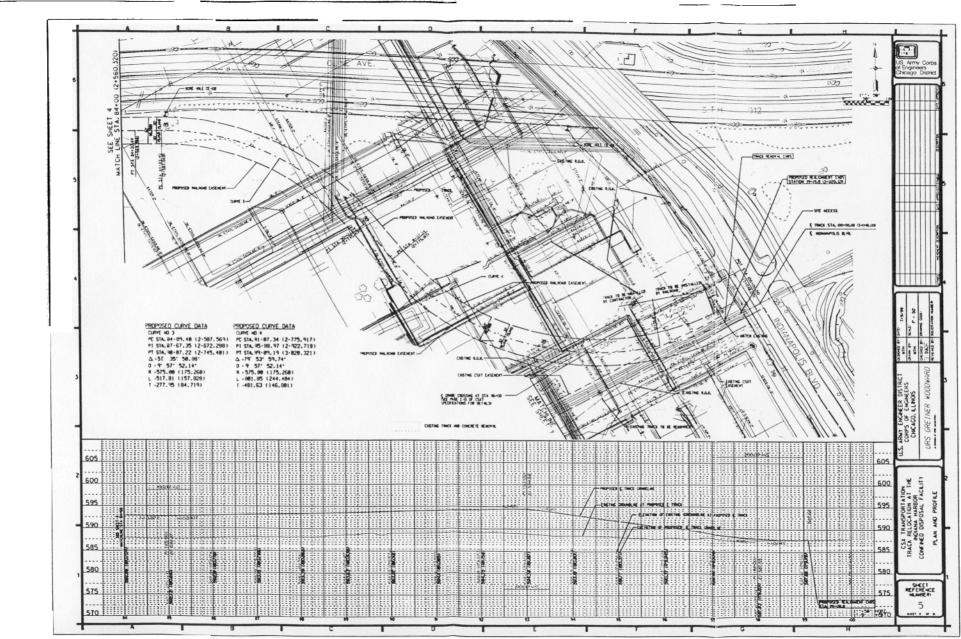


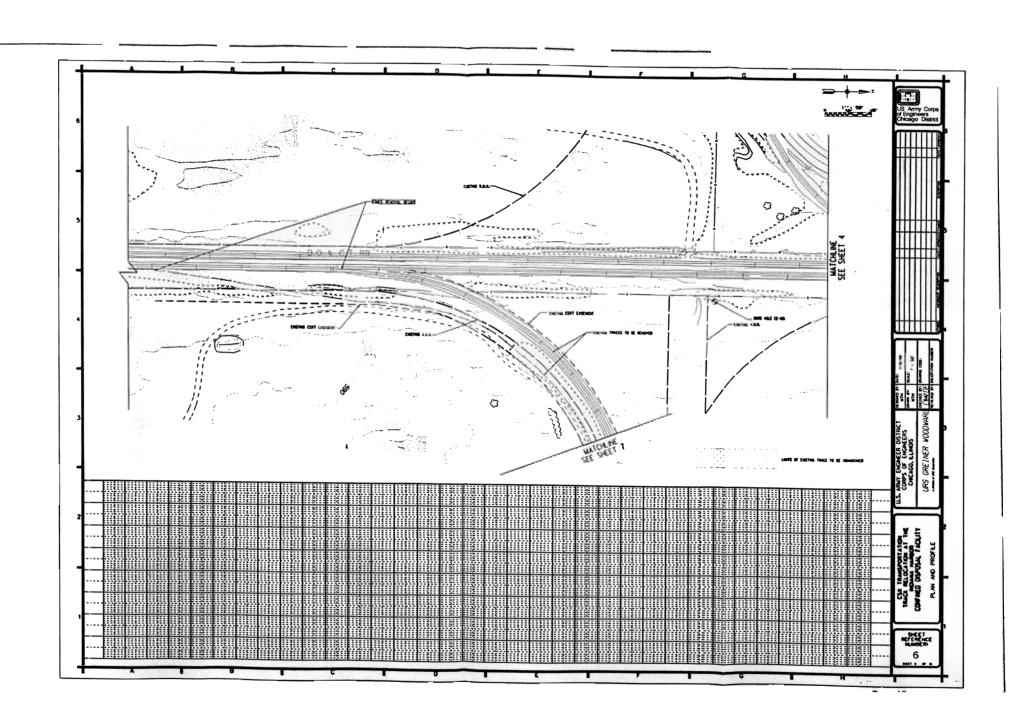






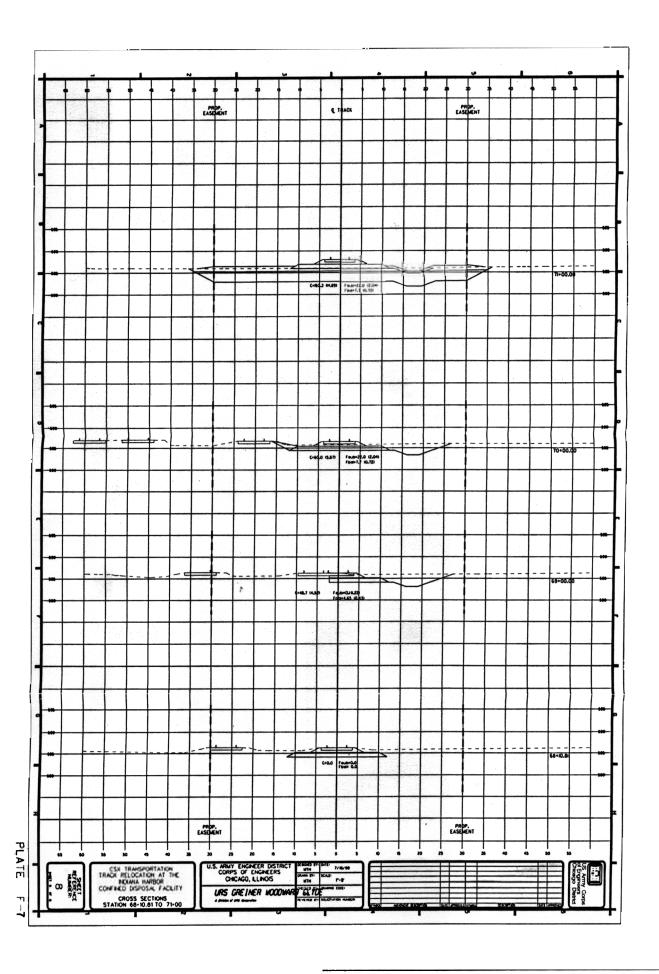


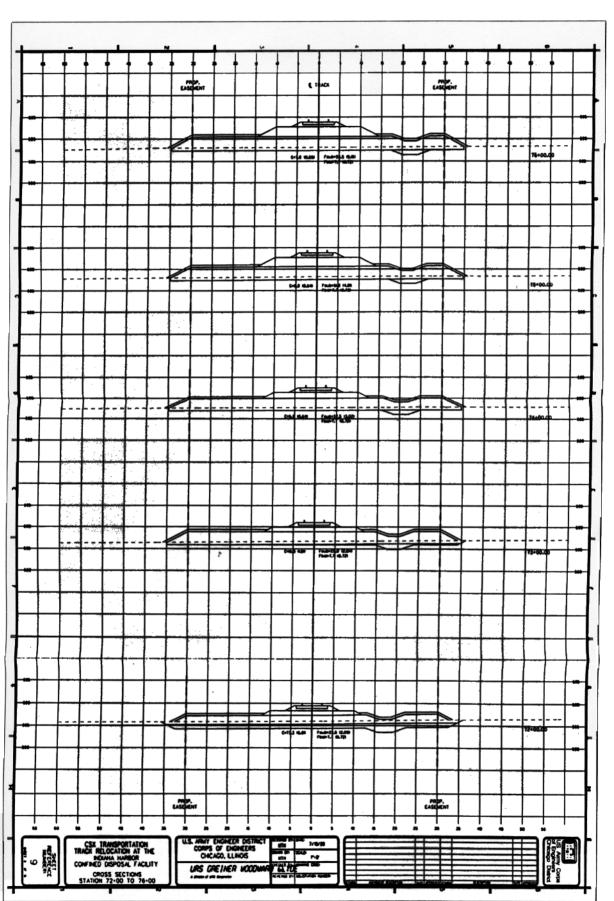




US Army Corp of Engineers Chicago Distric URS GREINER WOODWARD CSX TRANSPORTATION
TRACK RELUCATION AT THE
HODANA HARBOR
COMPRED DISPOSAL FACULTY
PLAN AND PROFILE SEET REFERENCE NUMBER 7

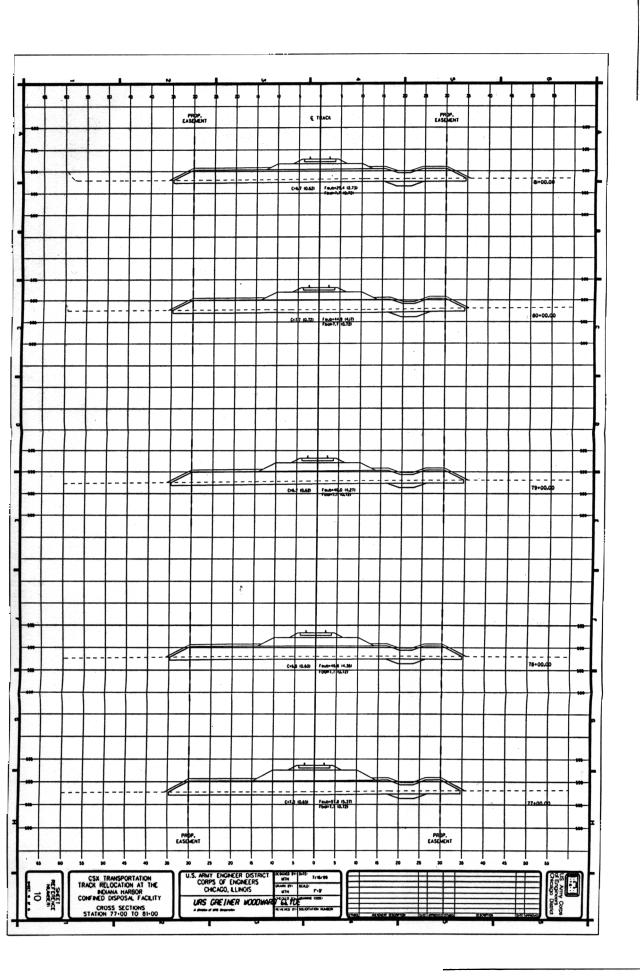
DIATE

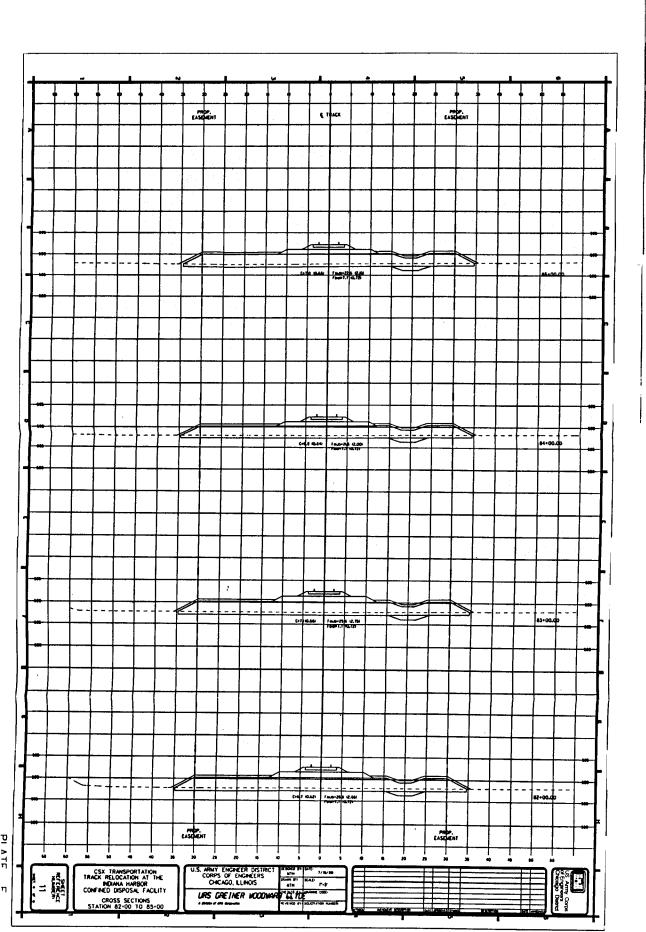


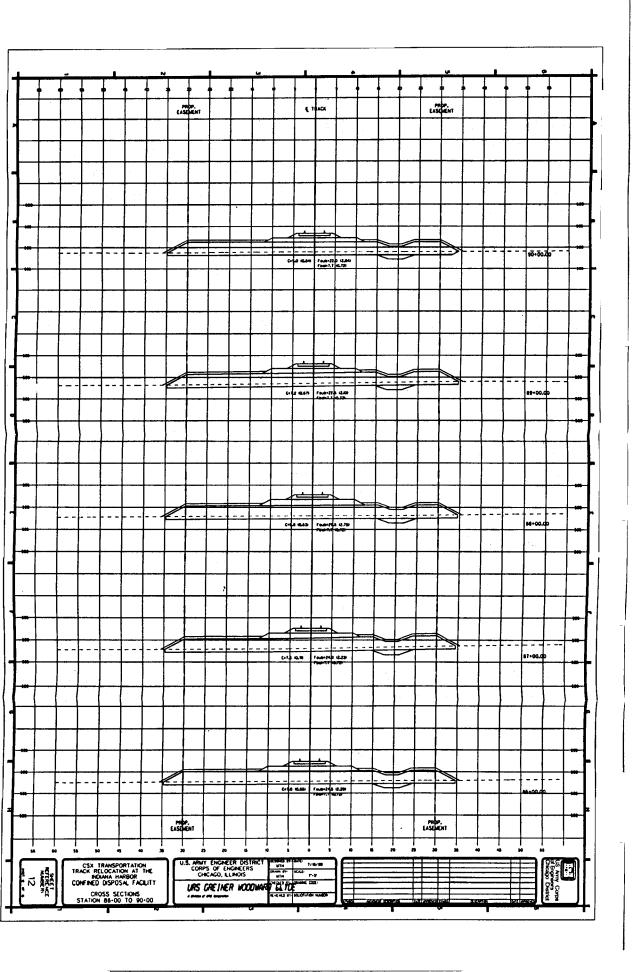


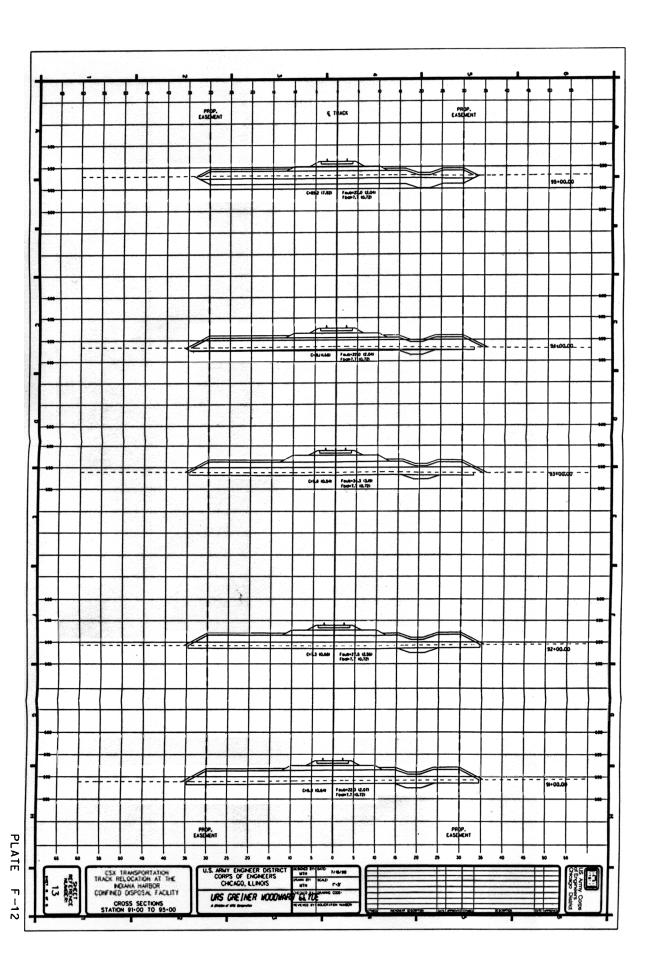
PLATE

E F-8









							
590					- 100 5 70 1 100 100	W f at any	590
585		TO SEA SEC ON SEC			H.F.K.		585
580							580
575		STATE OF STATE OF	in the Table That David.		ACCUPATION CONTRACTOR		575
570		STEP STORY CALL STURING	DEC. SING				
565	護						570
	能		T T	THE CAT IT ELV. SAS	2	86 86	565
560	SET PAI SET CLU, THE	第		選	CAT, SAILMAID	Be is the on	560
555	·	STATE OF THE CONTROL	REGION OF THE LOW	Side of Calary and	Auston, edi		555
550	D 10 F 100 C 101.004				DB # 8000 001.50		550
545	4		DR ST JONE D.C. SHA			134	545
540	,			DE S. 1896. D.D. 1405			540
535	3						535
530	,						530
525							Name of the
520							525
							520 515
515				# # # # # # # # # # # # # # # # # # #			515
510		AND THE TOTAL THE TANK THE PARTY OF THE PART					510 505
505		Acres 4					505
500)						500
495	ß						495
490)	an gre					490
485		STATE OF THE PROPERTY OF THE P					
480				1772			485
		COLUMN DIV. (N.D.					480
475		DD # 1000 D. D. 414.0					475
470	BORING CE-IO5	BORING CE-IO3	BORING CE-IO2	BORING CE-IOI	BORING CE-IO8		470



